



# Using Partial Pressure in Vacuum Furnaces

It is of primary importance to understand vapor pressure in the vacuum heat treatment of metals. Operating in vacuum can often lead to significant evaporation, or “boiling away,” of elemental constituents in the materials being processed, affecting surface integrity and in some cases altering the chemical composition of the base (or filler) metal. One way to overcome this problem is to introduce a gas partial pressure higher than that of the material’s vapor pressure. Different gas choices, introduction methods and controls are available to the heat treater. The natural questions are how and when should they be used? Let’s learn more.



### Vapor pressure

The vapor pressure of a material is the partial pressure present in the atmosphere which surrounds it. In other words, the vapor pressure tells us how much vapor a material will produce; a high vapor pressure means that the material will readily evaporate. Every material has a characteristic vapor pressure associated with it, which varies with temperature; the vapor pressure increases with increasing temperature.

All metals evaporate as a function of temperature (first-order effect) and vacuum level (second-order effect). Equation 1 allows the determination of the evaporation rate ( $Q$ ), and shows that the vapor pressure/temperature relationship is nearly logarithmic:

$$Q_{\max} = 0.058 P_v \sqrt{\frac{M}{T}}$$

where  $Q_{\max}$  = evaporation rate ( $\text{g}/\text{cm}^3\text{-sec}$ ),  $P_v$  = vapor pressure (torr),  $T$  = temperature (K) and  $M$  = molecular weight.

In vacuum furnaces, metals tend to volatilize at temperatures below their melting points. Table 1 shows this relationship for a number of common metals. The longer parts are held at the temperature and at the vacuum level shown, the greater the loss of the metallic element by evaporation. Where the element is part of a metal alloy system the vapor-pressure relationship changes (total vapor pressure of the alloy is the sum of the vapor pressures of each constituent times the percentage in the alloy, although this relationship has been debated by those knowledgeable in the field).

For example, processing aluminum, cadmium, magnesium, manganese and zinc or their alloys at temperatures as low as 400°C (750°F) may be marginally or totally impractical. This is why processing brass (Cu-Zn alloy) is normally not done in a vacuum system, or if it is, it is carried out at partial pressures near atmospheric. As the temperature increases, fewer materials can be run without being affected.

Stainless and tool steels and more exotic alloys often are processed in vacuum. Chromium present in these materials evaporates noticeably at temperatures and pressures within normal heat treatment ranges. Processed above 990°C (1815°F), chromium will vaporize if the vacuum level is less than  $1 \times 10^{-4}$  torr and the parts are held for a prolonged time. Heat treaters often observe a greenish discoloration (chromium oxide) on the interior of their vacuum furnaces, the result of chromium vapor reacting with air leaking into the hot zone. Otherwise, the evaporation deposit is bright and mirror-like. To avoid this, an operating partial pressure between 0.3 and 5 torr is typical for most chromium-containing parts.

For vacuum brazing (silver, copper, nickel), depletion of the filler metal alloy can be avoided by raising the pressure in the furnace to a level above the vapor pressure of the alloy at brazing temperature. For example, copper, having an equilibrium vapor pressure at 1120°C (2050°F) of  $1 \times 10^{-3}$  torr is usually run at a partial pressure between 1 and 10 torr. Nickel brazing normally is done in the  $10^{-3}$  to  $10^{-4}$  torr range. However, in the  $10^{-5}$  to  $10^{-6}$  torr range, you run the risk of losing some nickel, which has an equilibrium vapor pressure of  $1 \times 10^{-4}$  torr at 1190°C (2175°F).

### Which gases can we use?

Argon, hydrogen and nitrogen are the most common partial pressure gases. Often, argon is preferred as it tends to “sweep” the hot zone; that is, the heavy molecule tends to reduce evaporation compared with nitrogen and hydrogen. Specialized applications such as those in the electronics industry may use



Load of flat-plate heat exchangers ready for brazing at 5 torr nitrogen partial pressure at 1120°C. Photo courtesy of Solar Atmospheres Inc.



helium or even neon (if an ionizing gas is needed). Gases having a minimum purity of 99.99% and a dew point of -60°C (-76°F) or lower should be specified.

Certain cautions are in order. For example, nitrogen may react with certain stainless steels and titanium-containing materials resulting in surface nitriding. In the case of hydrogen, the normally near neutral vacuum atmosphere can be sharply shifted to a reducing atmosphere to pre-

vent oxidation of sensitive process work or for furnace/fixture bakeout/cleanup cycles. Embrittlement by hydrogen is a concern for certain materials (e.g., Ti, Ta).

### Measurement and control

It is critical to know the exact pressure, flow and type of gas being injected into the vacuum furnace so the process being run is under control. Thermocouple gages typically found on vacuum furnaces are affect-

ed by gas species, because they are calibrated for air. It is not uncommon to believe, for example, that you are running an argon partial pressure at 1 torr when in reality you are running at 0.4 torr, or with hydrogen (or helium) that you are at 10 torr when you are really at 1 torr. Absolute-pressure gages, such as the BOC Edwards Barocel® (Wilmington, Mass.; www.boc-edwards.com/industrial) should be used to determine precise partial pressure values.

For flow accuracy, flowmeters should have a micrometer needle valve installed in the downstream line. On many units, the gas is pulsed in using a solenoid valve and set-point control on the vacuum gage, similar to continuous flow with a needle valve installed. Also, it is extremely important to inject the partial pressure gas directly into the hot zone so the gas does not short circuit the work area.

### Summary

Partial pressure atmospheres are required in many heat treating and brazing operations to achieve the desired results. Introduction of the partial pressure gas into the furnace hot zone at one or more locations and controlling the partial pressure injection gas stream as a continuous flow rather than trying to operate at a specific pressure are critical considerations. The choice of partial pressure gas is also important both from a cost and quality standpoint. **IH**

### Bibliography

- Jones, W.R., Partial Pressure Vacuum Processing – Part I and II, *Ind. Htg.*, Sept./Oct., 1997
- *Vacuum Technology: Practical Heat Treating and Brazing*, R. Fabian, Ed., ASM Intl, 1993
- Practical Vacuum Systems Design, The Boeing Company
- William Jones, Solar Atmospheres Inc., private correspondence
- R. Houghton Jr., Hayes Heat Treating, private correspondence

Additional related information may be found by searching for these (and other) key words/terms via BNP Media LINX at [www.industrialheating.com](http://www.industrialheating.com): vacuum furnace, vacuum heat treating, vacuum brazing, vapor pressure, partial pressure, evaporation rate.

Table 1 Vapor pressures for selected elements

Element	Temperature (°C) at which specific vapor pressure (torr) exists						
	0.001	0.01	0.1	1.0	10	100	760
Al	889	996	1123	1279	1487	1749	2327
Be	1029	1212	1367	1567	1787	2097	2507
B	1239	1355	1489	1648	3030	3460	2527
Cd	220	264	321	394	484	611	765
Ca	528	605	700	817	983	1207	1482
C	2471	2681	2926	3214	3946	4373	4552
Cr	1090	1205	1342	1504	-	-	2222
Co	1494	1649	1833	2056	2380	2720	3097
Cu	1141	1273	1432	1628	1879	2207	2595
Ga	965	1093	1248	1443	1541	1784	2427
Ge	1112	1251	1421	1635	1880	2210	2707
Au	1316	1465	1646	1867	2154	2521	2966
Fe	1310	1447	1602	1783	2039	2360	2727
Pb	625	718	832	975	1167	1417	1737
Mg	383	443	515	605	702	909	1126
Mn	878	980	1103	1251	1505	1792	2097
Hg	18	48	82	126	184	216	361
Mo	2295	2533	2880	3102	3535	4109	4804
Nd	1192	1342	1537	1775	2095	2530	3090
Ni	1371	1510	1679	1884	2007	2364	2837
Pd	1405	1566	1759	2000	2280	2780	3167
P	160	190	225	265	310	370	431
Pt	1904	2090	2313	2582	3146	3714	3827
K	161	207	265	338	443	581	779
Re	2790	3060	3400	3810	-	-	5630
Rh	1971	2149	2358	2607	2880	3392	3877
Se	200	235	280	350	430	550	685
Si	1223	1343	1585	1670	1888	2083	2477
Ag	936	1047	1184	1353	1575	1865	2212
Na	238	291	356	437	548	696	914
S	66	97	135	183	246	333	444
Ta	2820	3074	3370	3740	-	-	6027
Sn	1042	1189	1373	1609	1703	1968	2727
Ti	1384	1546	1742	1965	2180	2480	3127
U	1730	1898	2098	2338	-	-	3527
V	1725	1888	2079	2207	2570	2950	3527
Zn	292	343	405	487	593	736	907
Zr	1818	2001	2212	2459	-	-	3577